HYBRID PREDICTIVE OUTPUT FEEDBACK STABILIZATION OF CONSTRAINED LINEAR SYSTEMS

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INTRODUCTION

• Input constraints:

- $\diamond\,$ Finite capacity of control actuators
- $\diamond\,$ Impose fundamental limitations on initial conditions
- Main issues for an effective control policy:
 - $\diamond\,$ Synthesis of stabilizing feedback laws
 - $\diamond\,$ Explicit characterization of set of admissible initial conditions
- Direct methods for control with constraints:
 - \diamond Bounded control
 - \star Constraint handling via explicit characterization of stability region
 - $\diamond\,$ Model predictive control
 - \star Constraint handling within open-loop optimal control setting
 - \star Successful applications in industry

LINEAR SYSTEMS WITH INPUT CONSTRAINTS

• State space description:

$$\begin{aligned} \dot{x}(t) &= Ax(t) + Bu(t) \\ y(t) &= Cx(t) \\ u(t) &\in \mathcal{U} \end{aligned}$$

 $x(t) \in \mathbb{R}^n$: state vector
 $u(t) \in \mathbb{R}^m$: control input
 $y(t) \in \mathbb{R}^k$: output vector
 (C, A): observable pair
 $y(t) \in \mathbb{R}^k$: output vector
 $0 \in \text{int. } \mathcal{U}$: compact & convex

• Finite parameterization of controls:

 $◊ U_{\Delta}$: piecewise constant functions (with period Δ & values in \mathcal{U}) $◊ u(·) ∈ U_{\Delta}$ characterized by sequence:

 $\{u[k]\}:\ u(t)=u(k\Delta),\ \forall\ t\in[k\Delta,(k+1)\Delta]$

• Stabilization of origin under constraints

MODEL PREDICTIVE CONTROL

• Control problem formulation

 \star Finite-horizon optimal control:

$$P(x,t) : \min\{J(x,t,u(\cdot)) | u(\cdot) \in U_{\Delta}\}$$

 \star Performance index:

$$J(x,t,u(\cdot)) = F(x(t+T)) + \int_{t}^{t+T} \left[\|x^{u}(s;x,t)\|_{Q}^{2} + \|u(s)\|_{R}^{2} \right] ds$$

- $\diamond \| \cdot \|_Q$: weighted norm
- $\diamond T$: horizon length
- \star Implicit feedback law

$$M(x) = u^0(t; x, t)$$

"repeated on-line optimization"

♦ Q, R > 0 : penalty weights
♦ $F(\cdot)$: terminal penalty



MODEL PREDICTIVE CONTROL

Formulations for closed-loop stability:

(Mayne et al, Automatica, 2000)

- \diamond Adjusting horizon length, terminal penalty, weights, etc.
- \diamond Imposing stability constraints on optimization:
 - \star Terminal equality constraints: (a)
 - * Terminal inequality constraints: $(x(t+T) \in W)$
 - \star Control Lyapunov function

$$x(t+T) = 0$$

s:
$$x(t+T) \in W$$

ns:
$$V(x(t+T)) < V(x(t))$$

- Issues of practical implementation:
 - \diamond Lack of (a priori) explicit characterization of stability region
 - \star Extensive closed-loop simulations
 - \star Restriction to small neighborhoods around origin

BOUNDED LYAPUNOV-BASED CONTROL

• Explicit bounded nonlinear control law:

$$u = -k(x, u_{max})(L_G V)^T$$

 \diamond An example gain: (Lin & Sontag, 1991)

$$k(x, u_{max}) = \left(\frac{L_f V + \sqrt{(L_f V)^2 + (u_{max} \| (L_G V)^T \|)^4}}{\| (L_G V)^T \|^2 \left[1 + \sqrt{1 + (u_{max} \| (L_G V)^T \|)^2}\right]}\right)$$
$$V = x^T P x, \ A^T P + P A - P B B^T P < 0$$

$$L_f V = x^T (A^T P + P A) x, \quad L_G V = 2x^T P B$$

♦ Nonlinear gain-shaping procedure:

 \star Accounts explicity for constraints & closed-loop stability

• Constrained closed-loop properties:

 $\diamond \ Asymptotic \ stability \qquad \diamond \ Inverse \ optimality$

$$J = \int_0^\infty (l(x) + u^T R(x)u) dt, \ l(x) > 0, \ R(x) > 0, \ J_{min} = V(x(0))$$

CHARACTERIZATION OF STABILITY PROPERTIES

$$D(u_{max}) = \{ x \in \mathbb{R}^n : L_f V < u_{max} | (L_G V)^T | \}$$

• Properties of inequality:

 $\diamond\,$ Describes open unbounded region where:

$$\triangleright |u| \le u_{max} \quad \forall \ x \in D$$

- $\triangleright \ \dot{V} < 0 \ \forall \ 0 \neq x \in D$
- ♦ Captures constraint-dependence of stability region
- $\diamond~D$ not necessarily invariant
- Region of guaranteed closed-loop stability:

$$\Omega(u_{max}) = \{x \in \mathbb{R}^n : V(x) \le c_{max}\}$$

- ♦ Region of invariance: $x(0) ∈ Ω \implies x(t) ∈ Ω ⊂ D ∀ t ≥ 0$
- ♦ Provides larger estimate than saturated linear/nonlinear controllers

HYBRID CONTROL: UNITING BOUNDED CONTROL & MPC

(El-Farra, Mhaskar & Christofides, Automatica, 2004)

- Objectives:
 - ♦ Development of a framework for uniting the two approaches:
 - ▷ Reconcile tradeoffs in stability and optimality properties
 - \star Explicit characterization of constrained stability region
 - \star A safety net for the implementation of MPC
- Central idea:

Decoupling "optimality" & "constrained stabilizability"

- \diamond Stability region provided by bounded controller
- \diamond Optimal performance supplied by MPC controller
- Approach:
 - \diamond Switching between MPC & bounded controller

OVERVIEW OF HYBRID CONTROL STRATEGY



- Hierarchical control structure
 - $\star \text{ Plant level } \star \text{ Control level}$
- ★ Supervisory level
- Any MPC formulation can be used
 - \star Switching rules may vary
- Several switching schemes possible

CONTROLLER SWITCHING SCHEMES "STATE FEEDBACK"

• Stability-based switching:





• Feasibility-based switching:

(Stabilizing MPC formulations) $u_{\sigma}(x(t)) = \left\{ \begin{array}{c} b(x(t)), \ 0 \leq t < T^{*} \\ M(x(t)), \ t \geq T^{*} \end{array} \right\}$

 \star T^{*} : earliest time for which MPC yields feasible solution



IMPLICATIONS OF SWITCHING SCHEME

- A safety net for implementing MPC:
 - ♦ Bounded controller provides a fall-back mechanism
 - \diamond Switched closed-loop system inherits the stability region
 - ★ A priori guarantees for all $x(0) \in \Omega(u_{max})$
 - * Stability independent of MPC properties (e.g., horizon length)
 - $\star\,$ Can reduce computational load
- Conceptual differences from other schemes:
 - \diamond Switching does not occur locally
 - \diamond Provides stability region explicitly
 - $\diamond\,$ No switching occurs if switching rules are satisfied
 - \star Only MPC is implemented \Longrightarrow optimal performance recovered

STATE ESTIMATION & OUTPUT FEEDBACK CONTROL

- Lack of full state measurements:
 - ♦ Inaccessibility of some process variables for measurement.
 - $\diamond\,$ Estimation of states from measured outputs necessary.
- Main objectives for output feedback controller design:
 - ♦ To establish guaranteed stability from an explicitly characterized set of initial conditions:
 - ▷ Design technique for the state estimator.
 - ▷ Devise switching rules, based on available state measurements.
 - $\diamond\,$ Controlled rate of convergence of state estimation error.
- Approach for output feedback controller design:
 - \diamond Relies on separation principle: combination of
 - $\triangleright\,$ State feedback controllers.
 - \triangleright State observers.

DESIGN OF STATE OBSERVER

• State space description of estimator:

$$\dot{\hat{x}}(t) = A\hat{x}(t) + Bu(t) + L(y - C\hat{x})$$

 $\diamond \hat{x}$: state estimate.

 $\diamond~L:$ Observer gain matrix.

- Structural features:
 - ♦ Observer pole placement:
 - ▷ Enforce desired decay of estimation error
 - $\diamond\,$ Effect of observer peaking eliminated through:
 - \triangleright Input saturation (indirect), OR
 - ▷ Estimate-saturation (direct)(e.g., El-Farra & Christofides, IJC, 2001).
- Closed-loop analysis:
 - ♦ Fall back (bounded controller) robust to a certain allowable error.
 - $\diamond\,$ For a given choice of initial conditions:
 - ▷ State estimator designed to force error under the allowable error.
 - ▷ Switching laws, based on the state estimates, for "safe" MPC implementation.

STATE ESTIMATION & OUTPUT FEEDBACK CONTROL

• Practical implications:

- Any other estimation scheme, such as Moving Horizon Estimation (MHE), can be used.
- ◊ Requires a transparent relationship between error decay and estimator parameters.
- ♦ MPC implemented in a region where the fall back controller can step in any time to rescue stability.



OUTPUT FEEDBACK IMPLEMENTATION OF SWITCHING (Mhaskar, El-Farra, & Christofides, AIChE J., to appear)

- Bounded controller design $(u = -k(x)L_gV, \ \Omega(u_{max})).$
- State observer design (given $\Omega_b \subset \Omega$, compute L).
- Estimate 'safe' region (given $\hat{x} \in \Omega_s \Rightarrow x \in \Omega$).
- Initialize: $\hat{x}(0) \in \Omega_b$, $u(0) = b(\hat{x}(0))$.
- After \hat{x} enters 'safe' region, Ω_s , check feasibility of MPC & implement if $\dot{V}(\hat{x}) < 0$ else keep bounded controller active.



SIMULATION EXAMPLE

• State-space description:

$$\dot{x}(t) = Ax(t) + Bu(t)$$
$$y(t) = Cx(t)$$

$$A = \begin{bmatrix} 0.55 & 0.15 & 0.05 \\ 0.15 & 0.40 & 0.20 \\ 0.10 & 0.15 & 0.45 \end{bmatrix}, B = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 1 & 1 \end{bmatrix}, C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

- * Origin unstable (three real positive eigenvalues)
- * Input constraints: $u_i \in [-1, 1], i = 1, 2$
- \star Only the first and the third states are measured

CONTROLLER DESIGN

• Bounded controller:

 $\diamond\,$ Lyapunov function:

$$V = x^T P x, P = \begin{bmatrix} 6.5843 & 4.2389 & -3.8307 \\ 4.2389 & 3.6091 & -2.6672 \\ -3.8307 & -2.6672 & 2.8033 \end{bmatrix}$$

 \diamond Stability region: $x^T (A^T P + P A) x < ||B^T P x||$

• Model predictive controller:

♦ Performance index:

$$J = \int_{t}^{t+T} \left[\|x(\tau)\|_{Q}^{2} + \|u(\tau)\|_{R}^{2} + \|\dot{u}(\tau)\|_{S}^{2} \right] d\tau$$

 $Q = qI > 0, \ R = rI > 0, \ S = sI > 0$

• State observer: $(\lambda = 500, a = 2)$

CLOSED-LOOP SIMULATION RESULTS

* State & estimate profiles

 \star Input profiles





CLOSED-LOOP SIMULATION RESULTS

 \star State & estimate profiles





- \star Observer gain: $\lambda = 0.5$
- ★ Bounded controller
 (MPC infeasible, no switching)

CONCLUSIONS

- Output feedback stabilization of constrained linear systems
- A hybrid control structure uniting MPC & bounded control
 - \diamond Decoupling:
 - \star Optimality (model predictive control)
 - \star Constrained stability region (bounded control)
 - ♦ Output feedback implementation of switching strategy:
 - \star State feedback controller design
 - \star State observers
 - $\diamond~{\rm A}$ safety net for implementation of MPC

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